Codebook Design and Performance Analysis of Quantized Beamforming under Perfect and Imperfect Channel State Information

Samuel T. Valduga, André L. F. de Almeida, Renato Machado, Andrei P. Legg, Murilo B. Loiola and Dimas I. Alves

Abstract-This paper presents a codebook design to multiple transmit and multiple receive antenna system with quantized feedback channel. The codebook design is based on trigonometrical expressions that give a quasi-orthogonal structure to the codes. The codebook is designed to a specific number of transmit antennas and can easily be adapted to different number of feedback bits. An instantaneous signalto-noise ratio analysis is performed which is used to optimize the codebooks. An upper bound on the bit error rate (BER) performance for the proposed scheme is provided as well. We also investigate the system performance under more realistic conditions, and for this purpose we consider a time-varying and spatially-correlated channel model. We compare the BER performance of the proposed scheme with other closed-loop codebook-based schemes. Results show that the proposed scheme outperforms other good schemes in terms of array gain.

Index Terms—MIMO, beamforming, quantized feedback, BER and channel estimation.

I. INTRODUCTION

Quantized transmit beamforming is an interesting solution for multiple input multiple output (MIMO) systems since the directional signal can improve the signal-to-noise ratio (SNR) at the receiver enhancing the channel capacity [1] and reducing the bit error probability of the system [2]. For a quantized feedback system, a performance enhancement will depend on the system design and, obviously, on the available feedback information. When analog full channel state information (CSI) is available to the transmitter, optimal *beamforming* is the best strategy to be considered [3].

Deployment of multiple antennas is normally associated with high costs since multiple antennas usually require

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an equal number of radio frequency (RF) chains (transmit amplifiers, modulators, etc.), which are expensive and powerconsuming. To circumvent this problem, a subset of the available antennas can be selected, thereby reducing the number of RF chains. The amount of feedback required in this case is much smaller. Such an approach is called *transmit antenna selection* (TAS). The most well-known TAS scheme was proposed by Gore and Paulraj [4] and later an extension of this idea was presented in [5]. Another interesting way of using the feedback information is by considering codebookbased (CBB) designs, where the feedback information is used to select a codeword from a finite codebook [2].

Along the last years, several works have investigated the use of quantized feedback in multiple-antenna systems [6]–[14]. Codebook design techniques based on Grassmann and Grassmannian-Stiefel manifold were proposed in [6], [7], where the main idea was to optimize the use of the quantized space of the eigendirections for MIMO channels. In the same direction, other codebook designs could be mentioned, such as random vector quantization (RVQ), discrete Fourier transform (DFT), and Lloyd codebooks, where a comparative analysis among them can be found in [8].

A class of extended orthogonal space-time block codes (EO-STBCs) for MIMO channels considering four transmit antennas over quasi-static flat fading channels was proposed in [9]. The spatial transmission rate those codes is unitary, since two symbols are transmitted over two periods of symbol. Based on the feedback information, a preprocessing is performed where the phases of the transmit symbols are rotated in a way to maximize the instantaneous SNR. As a result, the EO-STBC outperformed previous rate-one closedloop STBCs with four transmit antennas. Zhu et al. presented an analysis on symbol error rate (SER) of maximum ratio transmission, transmit antenna selection, and codebook-based beamforming in correlated Rayleigh fading channels [10]. They have derived an upper bound on the average SER of those schemes for a quantized CSI. Choi et al. proposed another phase-feedback-assisted scheme with four transmit antennas which uses a preprocessor to combine two Alamouti codes aiming at the Frobenius norm maximization [11]. They showed that full diversity is achieved by the combination made through preprocessing. Moreover, the feedback information was used to increase the coding gain. Herein, we refer to this scheme as Alamouti-code based scheme (ACBS).

Transmit beamforming codebooks with separate amplitude and phase quantization was presented in [12]. The aim is either to maximize transmission rate (egoistic beamforming) or to minimize co-channel interference (altruistic beamforming). In [13] a MIMO scheme based on quasi-orthogonal spacetime block code (QOSTBC) for four transmit antennas was proposed. The idea is to eliminate the cross interference terms using the transmit antenna shuffling. Thus, an optimum antenna shuffling pattern is selected to improve the transmit diversity with limited feedback information over four time slots (modulation instants). However, this scheme was already outperformed by [9] in terms of bit error rate (BER) performance. Furthermore, some approaches considering precoding codebook based on the well-know DFT matrices are found in [14], where the main contribution is the lowcomplexity of the codebooks since the pre-processing is based on simple trigonometrical expressions.

In this context, we have proposed in [15] a codebook design for four-transmit-antenna quantized beamforming system. The codebook design is based on trigonometrical expressions that give a quasi-orthogonal structure to the codes. We also carried out an instantaneous SNR analysis which was taken into account to optimize the codebooks. Therein, an upper bound on the average BER performance is provided, which is used to show that the proposed scheme also achieves full diversity.

In this paper, the work presented in [15] is extended to a more general solution, where the proposed scheme is adjustable for any number of transmit antennas that is a multiple of four. Moreover, we assess the system performance under more realistic conditions, where a timevarying and spatially-correlated channel model [16] is adopted, and two channel estimation methods are considered [3], [17]. Additionally, the BER performance of the proposed scheme is compared with other closed-loop codebook-based schemes with four transmit antennas and unitary spatial transmission rate, which allows a more comprehensive performance evaluation.

The rest of the paper is organized as follows. Section II presents the system model. Section III addresses the proposed codebook design and the SNR analysis. In Section IV, an upper bound on the BER performance is derived. In Section V, we present the channel model considering Doppler and spatial correlation. In Section VI, we extend the proposal to MIMO for $M_T = 4N$ transmit antennas, and results are presented and discussed. Finally, Section VII presents some concluding remarks.

Throughout this paper, normal letters represent scalar quantities, boldface lowercase letters indicate vectors, and boldface uppercase letters indicate matrices. The superscripts 'T', '*', '(·)^H' represent the transpose, the complex conjugate and the conjugate transpose operation, $|\cdot|^2$ denotes the modulus squared of a complex number, $\Re\{\cdot\}$ the real part of a complex number and ' \odot ' is the Hadamard product.

II. SYSTEM MODEL

Consider a MIMO system with M_T antennas at the transmitter and M_R antennas at the receiver. The channel is

assumed to be quasi-static, flat Rayleigh fading, being constant over a frame and varying randomly from one frame to the next. The transmission model consists of a preprocessing based on trigonometrical expressions, which is given by

$$\mathbf{Y} = \sqrt{\rho} \mathbf{H} \mathbf{P} + \mathbf{N},\tag{1}$$

where \mathbf{Y} is the $M_R \times \tau$ matrix of received signals and \mathbf{P} is the $M_T \times \tau$ matrix of processed transmitted signals with unit average energy. Let $\mathcal{CN}(0, \mathbf{R})$ represent the joint probability density function (p.d.f.) of a zero-mean circularly symmetric complex normal random vector with covariance matrix \mathbf{R} . Then, \mathbf{N} is the $M_R \times \tau$ matrix $\mathcal{CN}(\mathbf{0}, \mathbf{I}_{\tau M_R})$ representing the joint p.d.f. of the independent and identically distributed (i.i.d.) additive Gaussian noise samples with unit variance, \mathbf{H} is the $M_R \times M_T$ MIMO channel characterized by the p.d.f. $\mathcal{CN}(\mathbf{0}, \mathbf{I}_{M_R M_T})$, and $\rho = E_b/N_0$, which is the SNR associated to each receive antenna. E_b is the average bit energy and N_0 is the noise variance.

We assume the information bits are mapped into a baseband unitary average energy constellation, such as PSK or QAM, giving rise to Q data symbols $\{s_q\}, q = 1, \ldots, Q$, to be transmitted over τ symbol periods. In this paper, we consider only schemes with unitary spatial transmission rate, i.e., $R = \frac{Q}{\tau} \log_2(M) = \log_2(M)$. In order to simplify the analytical derivations, we also assume that the channel coefficients are perfectly estimated at the receiver and that there is a reliable feedback channel through which b bits can be sent to the transmitter. In Section V we consider more realistic assumptions in order to assess the system performance under more realistic scenarios.

III. PROPOSED SCHEME

We start this section by considering the proposed transmission scheme for four transmit antennas as was presented in [15].

Assume that only one information symbol, s, is transmitted per transmit period. The symbol s is preprocessed by a complex transmission codeword **x**:

 $\mathbf{p} = s\mathbf{x}$

where

$$\mathbf{x} = \left[\left(\left[\begin{array}{cc} \cos(\theta)/\sqrt{2} & 0\\ 0 & \sin(\theta)/\sqrt{2} \end{array} \right] \otimes \mathbf{I}_2 \right) \mathbf{v}_{\varphi} \right], \\ = \frac{1}{\sqrt{2}} \left[\begin{array}{c} \cos(\theta)e^{j\varphi_0}\\ \cos(\theta)e^{j\varphi_1}\\ \sin(\theta)e^{j\varphi_2}\\ \sin(\theta)e^{j\varphi_2} \end{array} \right],$$

 \otimes is the Kronecker product, \mathbf{I}_2 is the 2-by-2 identity matrix, the factor $\frac{1}{\sqrt{2}}$ is used to normalize the transmit power and $\mathbf{v}_{\varphi} = \begin{bmatrix} e^{j\varphi_0} & e^{j\varphi_1} & e^{j\varphi_0} & e^{j\varphi_2} \end{bmatrix}^{\mathrm{T}}$. For simplicity of analysis, we assume that $\varphi_0 = 0$ and henceforth we follow with this assumption. It is worth mentioning that all of the analyses presented in this paper apply to any other $\varphi_0 \neq 0$.

Before each transmission takes place, the receiver feeds back b bits to the transmitter. The information is used by the preprocessor to choose the appropriate codeword, i.e., the

(2)

one that maximizes the instantaneous SNR, $\mathbf{x}_{\max} \in \mathbf{X} = [\mathbf{x}_1, \mathbf{x}_2, \dots, \mathbf{x}_N]$, where $N = 2^b$. As one can see, the codebook is a function of φ_1, φ_2 and θ , which are the variables that must be optimized to maximize the system performance.

Next, we present the receiver for M_R receive antennas, the SNR analysis, used to optimize φ_1 , φ_2 and θ in a unquantized space, and then the codebook design for $N = 2^b$.

A. Receiver for M_R receive antennas

From (1) and (2), the received signal \mathbf{y} for M_R receive antennas can be rewritten as

$$y = Hp + n,$$
 (3)
$$= sHx + n$$

$$= \bar{h} + n$$

where

$$\bar{\mathbf{h}} = s[h_{p1} \dots h_{pM_R}]^{\mathrm{T}},\tag{4}$$

in which

$$h_{pj} = \cos(\theta)h_{1,j} + \cos(\theta)e^{\varphi_1}h_{2,j}$$

$$+\sin(\theta)h_{3,j} + \sin(\theta)e^{\varphi_2}h_{4,j}$$
(5)

and

$$\mathbf{H} = \begin{bmatrix} h_{1,1} & h_{2,1} & h_{3,1} & h_{4,1} \\ \vdots & \vdots & \vdots \\ h_{1,M_R} & h_{2,M_R} & h_{3,M_R} & h_{4,M_R} \end{bmatrix}$$

where **n** is the $1 \times M_R$ ($\tau = 1$) additive white Gaussian noise vector, and $h_{i,j}$ denotes path gain from the *i*-th transmit antenna to the *j*-th receive antenna.

Considering the received signal in (4) and employing the maximal ratio combining (MRC) technique, the following processing produces the desired inputs to the maximum-likelihood detector:

$$\tilde{s} = \bar{\mathbf{h}}^{H} \mathbf{y}$$
(6)
$$= s \left[\left(\sum_{j=1}^{M_{R}} (|h_{1,j}|^{2} + |h_{2,j}|^{2}) + \beta_{c} \right) \cos(\theta)^{2} + \left(\sum_{j=1}^{M_{R}} (|h_{3,j}|^{2} + |h_{4,j}|^{2}) + \beta_{s} \right) \sin(\theta)^{2} + \beta_{cs} \cos(\theta) \sin(\theta) \left] \sqrt{\rho} / 2 + \sum_{j=1}^{M_{R}} h_{pj}^{*} \eta_{j},$$

$$\beta_{c} = \sum_{j=1}^{M_{R}} \beta_{cj}, \quad \beta_{s} = \sum_{j=1}^{M_{R}} \beta_{sj}, \quad \beta_{cs} = \sum_{j=1}^{M_{R}} \beta_{csj},$$

$$\beta_{cj} = 2 \Re \left\{ h_{1,j} h_{2,j}^{*} e^{-j\varphi_{2}} \right\},$$

$$\beta_{csj} = 2 \Re \left\{ (h_{1,j} + h_{2,j} e^{j\varphi_{1}}) (h_{3,j} + h_{4,j} e^{j\varphi_{2}})^{*} \right\}.$$

B. SNR Analysis

For the signal obtained in (6), the instantaneous output SNR is given by

$$\gamma = \left(\frac{g_c \cos^2(\theta) + g_s \sin^2(\theta) + \beta_{cs} \cos(\theta) \sin(\theta)}{2}\right)\rho \quad (7)$$

where

$$g_{c} = \left[\sum_{j=1}^{M_{R}} |h_{1,j}|^{2} + |h_{2,j}|^{2} + 2\Re\{h_{1,j}h_{2,j}^{*}e^{-j\varphi_{1}}\}\right] \\ \times \cos^{2}(\theta),$$

$$g_{s} = \left[\sum_{j=1}^{M_{R}} |h_{3,j}|^{2} + |h_{4,j}|^{2} + 2\Re\{h_{3,j}h_{4,j}^{*}e^{-j\varphi_{2}}\}\right] \\ \times \sin^{2}(\theta),$$

$$\beta_{cs} = \sum_{j=1}^{M_{R}} 2\Re\{(h_{1,j} + h_{2,j}e^{j\varphi_{1}}) \\ \times (h_{3,j} + h_{4,j}e^{j\varphi_{2}})^{*}\}.$$

With (7), one can determine the optimal φ_1 , φ_2 , and θ by differentiation, which gives the maximum output SNR. Nevertheless, it is important to mention that full diversity can be achieved either with unquantized or quantized feedback channel, as described latter. From (7) we observe that there is a dependence between the variables. Thus, we decided to solve the problem in three steps. In the first step, we differentiate β_c and β_s with respect to φ_1 and φ_2 , respectively, and set them both equal to zero. We can easily verify that those terms are maximized when

$$\varphi_1 = \arctan\left(\sum_{j=1}^{M_R} \frac{\sin(\xi_{1,j} - \xi_{2,j})\alpha_{1,j}\alpha_{2,j}}{\cos(\xi_{1,j} - \xi_{2,j})\alpha_{1,j}\alpha_{2,j}}\right)$$
(8)

$$\varphi_2 = \arctan\left(\sum_{j=1}^{M_R} \frac{\sin(\xi_{3,j} - \xi_{4,j})\alpha_{3,j}\alpha_{4,j}}{\cos(\xi_{3,j} - \xi_{4,j})\alpha_{3,j}\alpha_{4,j}}\right)$$
(9)

where, $h_{i,j} = \alpha_{i,j} \exp{\{\xi_{i,j}\}}$.

In the second and third steps, we differentiate (7) with respect to θ . The first and second derivatives are then given by

$$\gamma' = 2\kappa \left(\cos(\theta)\sin(\theta)\right) + \beta_{cs} \left(\cos^2(\theta) - \sin^2(\theta)\right)$$
$$\gamma'' = 2\kappa \left(\cos^2(\theta) - \sin^2(\theta)\right) - 4\beta_{cs} \left(\cos(\theta)\sin(\theta)\right), (10)$$

respectively, where $\kappa = g_s - g_c$. The third step is necessary to make sure that the solution is a maximum and not a minimum. The solving (10) under the conditions of $\gamma' = 0$ and $\gamma'' < 0$, we obtain the following optimal θ

$$\theta_{opt} = \arctan\left(\frac{\kappa + \sqrt{\kappa^2 + 2\beta_{cs}^2}}{\beta_{cs}}\right).$$
(11)

We decide to omit the term ρ in (10), since this condition does not cause any alteration in the final result.

C. Codebook Design

In this section we present how to perform the proposed scheme based on quantized feedback. We assume two uniform finite sets: φ_{1q} and $\varphi_{2q} \in [0, \pi]$ and $\theta_q \in [-\pi/2, \pi/2]$. Since the receiver needs to feed back the state information about two phases (φ_{1q} and φ_{2q}) and one angle (θ_q), the

minimum quantization is, therefore, b = 3 bits. The receiver computes and compares 2^b instantaneous SNR and send b bits through the feedback channel to inform which code from the codebook must be considered for transmission. This process is repeated before a new transmission takes place. The system configuration for b = 3 is presented in Table I.

TABLE ISystem configuration for b = 3. This is the minimumQUANTIZATION THAT YIELDS FULL DIVERSITY FOR THE PROPOSEDSCHEME

γ Parameters			Angle-Phases			Feedback bits			
β_c	β_s	β_{cs}	κ	θ_q	φ_{1q}	φ_{2q}	b_0	b_1	b_2
> 0	> 0	> 0	#	$\frac{\pi}{4}$	0	0	0	0	0
> 0	< 0	> 0	#	$\frac{\pi}{4}$	0	π	0	0	1
< 0	> 0	> 0	#	$\frac{\pi}{4}$	π	0	0	1	0
< 0	< 0	> 0	#	$\frac{\pi}{4}$	π	π	0	1	1
> 0	> 0	< 0	#	$-\frac{\pi}{4}$	0	0	1	0	0
> 0	< 0	< 0	#	$-\frac{\pi}{4}$	0	π	1	0	1
< 0	> 0	< 0	#	$-\frac{\pi}{4}$	π	0	1	1	0
< 0	< 0	< 0	#	$-\frac{\pi}{4}$	π	π	1	1	1

TABLE II System configuration for b = 4.

γ Parameters			Angle-Phases		Feedback bits					
β_c	β_s	β_{cs}	κ	θ_q	φ_{1q}	φ_{2q}	b_0	b_1	b_2	b_3
> 0	> 0	> 0	> 0	$\frac{3\pi}{8}$	0	0	0	0	0	0
> 0	< 0	> 0	> 0	$\frac{3\pi}{8}$	0	π	0	0	0	1
< 0	> 0	> 0	> 0	$\frac{3\pi}{8}$	π	0	0	0	1	0
< 0	< 0	> 0	> 0	$\frac{3\pi}{8}$	π	π	0	0	1	1
> 0	> 0	> 0	< 0	$\frac{\pi}{8}$	0	0	0	1	0	0
> 0	< 0	> 0	< 0	$\frac{\pi}{8}$	0	π	0	1	0	1
< 0	> 0	> 0	< 0	$\frac{\pi}{8}$	π	0	0	1	1	0
< 0	< 0	> 0	< 0	$\frac{\pi}{8}$	π	π	0	1	1	1
> 0	> 0	< 0	> 0	$\frac{-\pi}{8}$	0	0	1	0	0	0
> 0	< 0	< 0	> 0	$\frac{-\pi}{8}$	0	π	1	0	0	1
< 0	> 0	< 0	> 0	$\frac{-\pi}{8}$	π	0	1	0	1	0
< 0	< 0	< 0	> 0	$\frac{-\pi}{8}$	π	π	1	0	1	1
> 0	> 0	< 0	< 0	$\frac{-3\pi}{8}$	0	0	1	1	0	0
> 0	< 0	< 0	< 0	$\frac{-3\pi}{8}$	0	π	1	1	0	1
< 0	> 0	< 0	< 0	$\frac{-3\pi}{8}$	π	0	1	1	1	0
< 0	< 0	< 0	< 0	$\frac{-3\pi}{2}$	π	π	1	1	1	1

The symbol \sharp means "don't care state". Each row of Table I defines a codeword $\mathbf{x}(\varphi_1, \varphi_2, \theta)$. Phases φ_1 and φ_2 are used to keep β_c and β_s as non negative real numbers. As the number of feedback bits is increased, β_c and β_s will converge to the ideal (unquantized) solution, as presented in Section III-B. The angle θ is used to maximize the sum of the terms that compose the instantaneous SNR. The codebook is given by

$$\mathbf{X}_{8}^{4} = \begin{bmatrix} \cos(\pi/4) & \cos(\pi/4) & \sin(\pi/4) & \sin(\pi/4) \\ \cos(\pi/4) & \cos(\pi/4) & \sin(\pi/4) & \sin(\pi/4)e^{j\pi} \\ \cos(\pi/4) & \cos(\pi/4)e^{j\pi} & \sin(\pi/4) & \sin(\pi/4)e^{j\pi} \\ \cos(\pi/4) & \cos(\pi/4)e^{j\pi} & \sin(\pi/4) & \sin(\pi/4)e^{j\pi} \\ \cos(-\pi/4) & \cos(-\pi/4) & \sin(-\pi/4) & \sin(-\pi/4)e^{j\pi} \\ \cos(-\pi/4) & \cos(-\pi/4)e^{j\pi} & \sin(-\pi/4) & \sin(-\pi/4)e^{j\pi} \\ \cos(-\pi/4) & \cos(-\pi/4)e^{j\pi} & \sin(-\pi/4) & \sin(-\pi/4)e^{j\pi} \end{bmatrix}$$

Table II defines the system configuration for b = 4 and the respective codebook is given by \mathbf{X}_{16}^4 . The larger the

number of feedback bits, the better the codebook performance. To improve the BER performance we can increase the quantization of θ . On the other hand, by increasing the quantization of φ there is no considerable improvement in performance.

	$\int \cos(2\pi/8)$	$aaa(2\pi/8)$	$\sin(2\pi/8)$	$\sin(2\pi/8)$	ΙT
	$\cos(3\pi/8)$	$\cos(3\pi/8)$	$\sin(3\pi/6)$	$\sin(3\pi/6)$	
	$\cos(3\pi/8)$	$\cos(3\pi/8)$	$\sin(3\pi/8)$	$\sin(3\pi/8)e^{j\pi}$	
	$\cos(3\pi/8)$	$\cos(3\pi/8)e^{j\pi}$	$\sin(3\pi/8)$	$\sin(3\pi/8)$	
	$\cos(3\pi/8)$	$\cos(3\pi/8)e^{j\pi}$	$\sin(3\pi/8)$	$\sin(3\pi/8)e^{j\pi}$	
	$\cos(-3\pi/8)$	$\cos(-3\pi/8)$	$\sin(-3\pi/8)$	$\sin(-3\pi/8)$	
	$\cos(-3\pi/8)$	$\cos(-3\pi/8)$	$\sin(-3\pi/8)$	$\sin(-3\pi/8)e^{j\pi}$	
	$\cos(-3\pi/8)$	$\cos(-3\pi/8)e^{j\pi}$	$\sin(-3\pi/8)$	$\sin(-3\pi/8)$	
\mathbf{v}^4 –	$\cos(-3\pi/8)$	$\cos(-3\pi/8)e^{j\pi}$	$\sin(-3\pi/8)$	$\sin(-3\pi/8)e^{j\pi}$	
A ₁₆ -	$\cos(\pi/8)$	$\cos(\pi/8)$	$\sin(\pi/8)$	$\sin(\pi/8)$	
	$\cos(\pi/8)$	$\cos(\pi/8)$	$\sin(\pi/8)$	$\sin(\pi/8)e^{j\pi}$	
	$\cos(\pi/8)$	$\cos(\pi/8)e^{j\pi}$	$\sin(\pi/8)$	$\sin(\pi/8)$	
	$\cos(\pi/8)$	$\cos(\pi/8)e^{j\pi}$	$\sin(\pi/8)$	$\sin(\pi/8)e^{j\pi}$	
	$\cos(-\pi/8)$	$\cos(-\pi/8)$	$\sin(-\pi/8)$	$\sin(-\pi/8)$	
	$\cos(-\pi/8)$	$\cos(-\pi/8)$	$\sin(-\pi/8)$	$\sin(-\pi/8)e^{j\pi}$	
	$\cos(-\pi/8)$	$\cos(-\pi/8)e^{j\pi}$	$\sin(-\pi/8)$	$\sin(-\pi/8)$	
	$\cos(-\pi/8)$	$\cos(-\pi/8)e^{j\pi}$	$\sin(-\pi/8)$	$\sin(-\pi/8)e^{j\pi}$	

The feedback information, b_0, \ldots, b_{n-1} , is sent according to the rules defined for each system configuration. The codebook design for higher quantization.

IV. BER ANALYSIS

In this section, we present a BER analysis for the proposed codebook-based beamforming. The analysis is performed for PSK constellations. The BER of M-ary PSK constellation conditioned on the instantaneous SNR γ can be given by [18]:

$$BER(\gamma) = \frac{1}{\pi} \int_0^{\frac{(M-1)\pi}{M}} \exp\left(-\frac{C_m\gamma}{\sin^2(\theta)}\right) d\theta \qquad (12)$$

where M is the constellation size and $C_m = \sin^2(\pi/M)$. Taking the expectation over (12), the average BER can be written as

$$\overline{BER}(\gamma) = \mathbb{E}_h\{BER(\gamma)\},\tag{13}$$

where \mathbb{E}_h is the expectation operator with respect to h.

By assuming that the transmitter uses feedback information for choosing a codeword \mathbf{x} , which belongs to a certain finite codebook \mathbf{X} , such that the instantaneous SNR is maximized, we can rewritten (13) as

$$\overline{BER}(\rho) = \frac{1}{\pi} \int_0^{\frac{(M-1)\pi}{M}} \mathbb{M}\left(-\frac{C_m\rho}{\sin^2(\theta)}; \mathbf{X}\right) d\theta \qquad (14)$$

where $\mathbb{M}\left(-\frac{C_m\rho_x}{\sin^2(\theta)};\mathbf{X}\right)$ denotes the value of the function

$$\mathbb{M}(t; \mathbf{X}) \triangleq \mathbb{E}\left\{\exp\left(-t \max_{\mathbf{x} \in \mathbf{X}} |\mathbf{h}_p|^2\right)\right\}, t \ge 0$$

$$= \mathbb{E}\left\{\exp\left(-t \max_{\mathbf{x} \in \mathbf{X}} |\mathbf{H}\mathbf{x}|^2\right)\right\}, t \ge 0$$

$$(15)$$

As in [10], we consider the following approximation of (15):

$$\beta(\mathbf{X}) = \lim_{t \to \infty} t^{M_T M_R} \mathbb{M}(t; \mathbf{X})$$
(16)

in which the values assumed by $\beta(t, \mathbf{X})$ depend on the set of codewords in \mathbf{X} .

This asymptotic approximation is fundamental for our analysis since an exact expression is very hard to obtain. However, if the codebook is well designed, and that is the case here, then the codewords can be approximated by 'spherical caps' on the surface of hypersphere, which simplifies considerably the BER analysis [19].

Based on the results presented in [19] and [10] we have the following approximation of (16)

$$\beta(\mathbf{X}) = C_1 (M_T M_R - 1)! (M_T - 1)N$$

$$\times \sum_{n=0}^{M_T - 2} {M_T - 2 \choose n} \frac{(-1)^n (C_2^{-(M_T M_R - 1 - n)} - 1)}{M_T M_R - 1 - n}$$
(17)

where

$$C_1 = M_T M_R \prod_{n=1}^{\min(M_T M_R)} \frac{(\min(M_T M_R) - n)!}{(M_T M_R - 1)!}$$

and

$$C_2 = 1 - N^{\frac{-1}{M_T - 1}}.$$

A. An upper bound on the BER performance

In this section, we continue with the analysis of $\beta(\mathbf{X})$, whose result will be used in (14) culminating in an upper bound on the average BER. The normalized channel is defined by $\tilde{\mathbf{h}}_p \triangleq \frac{\mathbf{h}_p}{|\mathbf{h}_p|}$ where $|\mathbf{h}_p|$ is independent of its direction. Furthermore, since \mathbf{h}_p is Gaussian, $|\mathbf{h}_p|^2$ is a chisquare random variable with $2M_TM_R$ degree of freedom and has the following moment generating function (MGF) $\mathbb{E}\left\{\exp(-s|\mathbf{h}_p|^2)\right\} = (1+s)^{-M_TM_R}$.

Applying the MGF to (15), we obtain

$$\mathbb{M}(t; \mathbf{X}) = \mathbb{E}_{\tilde{\mathbf{h}}_{p}} \left\{ \mathbb{E}_{|\tilde{\mathbf{h}}_{p}|^{2}} \left\{ \exp\left[-(t\Omega|\tilde{\mathbf{h}}_{p}|^{2})|\mathbf{h}_{p}|^{2}\right] \right\} \right\}$$
$$= \mathbb{E}_{\tilde{\mathbf{h}}_{p}} \left\{ ((1+t\Omega)|\tilde{\mathbf{h}}_{p}|^{2})^{-M_{T}M_{R}} \right\}$$
(18)

where the subscript on the expectation operator indicates the random variable is being averaged over, and Ω is defined as

$$\Omega \triangleq \left(\max_{\mathbf{x} \in \mathbf{X}} |\tilde{\mathbf{h}_p}|^2 \right)^{-M_T M_R}.$$
(19)

Hence, we can rewrite (16) as

$$\beta(\mathbf{X}) = \lim_{t \to \infty} t^{M_T M_R} \mathbb{M}(t; \mathbf{X})$$

$$= \lim_{t \to \infty} t^{M_T M_R} \mathbb{E}_{\tilde{\mathbf{h}}_p} \left\{ \left(1 + \Omega^{\frac{-1}{M_T M_R}} \right)^{-M_T M_R} \right\}$$

$$= \mathbb{E}_{\tilde{\mathbf{h}}_p} \{ \Omega \}.$$
(20)

For t > 0, it is possible to affirm that $(1+t\Omega^{\frac{-1}{M_TM_R}})^{-M_TM_R}$ is concave with respect to Ω . Thus, applying Jensen's inequality to (18), yielding:

$$\mathbb{M}(t; \mathbf{X}) \leq \left\{ 1 + t \left(\mathbb{E}_{\tilde{\mathbf{h}}_{p}} \left\{ \Omega^{\frac{-1}{M_{T}M_{R}}} \right\} \right)^{-M_{T}M_{R}} \right\} \\
= \left\{ 1 + t \left(\beta(\mathbf{X})^{\frac{-1}{M_{T}M_{R}}} \right)^{-M_{T}M_{R}} \right\}.$$
(21)

Substituting (21) into (14), an upper bound on the average BER is obtained

$$\overline{BER}(\rho) \leq \frac{1}{\pi} \int_{0}^{\frac{(M-1)\pi}{M}} \left(1 + \frac{C\rho}{\sin^{2}(\theta)}\beta(\mathbf{X})^{\frac{-1}{M_{T}M_{R}}}\right)^{-M_{T}M_{R}} d\theta$$
(22)

It is clear that the diversity order of $M_T M_R$ is achieved.

V. OTHER SCENARIOS

The proposed scheme can also be employed in flat channels presenting time variation and/or spatial correlation. It is also important to evaluate the performance of the proposed technique when only imperfect channel state information (CSI) is available. Hence, in the next sections, we briefly describe the models we adopted for the two aforementioned channel effects, as well as the channel estimation techniques that provide the estimated CSI.

A. Time varying and spatially correlated channel model

In typical wireless communication systems, transmitters, receivers, and even the scatterers are not static, which may cause channel variation with time. This time variation is usually modeled as a wide-sense stationary stochastic process. Considering the well known Clark/Jakes fading model [18], [20], [21], the channel coefficients are modeled as independent, zero-mean, complex Gaussian random variables with time autocorrelation function

$$\mathbb{E}[h_{(i,j,k)}h_{(i,j,t)}^*] = \mathcal{J}_o(2\pi f_D T_s |k-t|),$$
(23)

where $h_{(i,j,k)}$ models the channel coefficient between the *i*-th transmit $(i = 1, ..., M_T)$ and *j*-th $(j = 1, ..., M_R)$ receive antennas at instant k, \mathcal{J}_o is the zero-order Bessel function of the first kind, $f_D T_s$ is the normalized Doppler rate (assumed the same for all of the transmit-receive pairs), T_s is the time interval needed to send one space-time codeword and f_D is the maximum Doppler shift, computed as $f_D = \frac{v \cdot f_c}{c}$ for a carrier frequency f_c , a relative velocity between transmitter and receiver of v m/s and the speed of light c.

From the time autocorrelation function (23), the normalized spectrum for each channel coefficient can be expressed as

$$S(f) = \begin{cases} \frac{1}{\pi f_D} \frac{1}{\sqrt{1 - \left(\frac{f}{f_D}\right)^2}}, & |f| < f_D \\ \sqrt{1 - \left(\frac{f}{f_D}\right)^2}, & 0, \\ 0, & \text{otherwise.} \end{cases}$$
(24)

It is important to highlight that this power spectrum characterizes isotropic channels, where the transmit antennas radiate uniformly in all directions.

Since the time autocorrelation function (23) is nonrational and its spectrum (24) is bandlimited, it is usual to develop approximations to those expressions for analysis, channel estimation, and simulation purposes. Hence, following [16], [22], [23], we herein approximate the time evolution of channel coefficients by first order auto-regressive, AR(1), processes due to their simplicity. This is possible since the first few correlation terms of (23), for small lags, capture most of the channel dynamics [23]. Therefore, the time-varying nature of each channel coefficient is given by

$$h_{(i,j,k)} = \beta h_{(i,j,k-1)} + w_k, \tag{25}$$

where $\beta = \mathcal{J}_o(2\pi f_D T_s)$ and w_k is an independent, circularly symmetric, zero-mean, Gaussian excitation noise with variance $\sigma_w^2 = (1 - \beta^2)$.

In the previous sections, all the channels in a MIMO system are supposed to be spatially uncorrelated. However, depending on the propagation environment, the polarization of the antenna elements and the spacing between them, spatial correlations may appear between channel coefficients. One of the most simple and used spatially correlated channel models splits the fading correlation into two independent components called receive correlation and transmit correlation, respectively. This channel model, called Kronecker model, can be written as [3]

$$\mathbf{H}_{k}^{\text{corr}} = \mathbf{R}_{M_{R}}^{1/2} \mathbf{H}_{k} \mathbf{R}_{M_{T}}^{1/2}, \qquad (26)$$

where $\mathbf{H}_{k}^{\text{corr}}$ represents a MIMO channel with spatially correlated coefficients, $\mathbf{R}_{M_{R}}$ and $\mathbf{R}_{M_{T}}$ model the correlation between receive and transmit antennas, respectively, $(\cdot)^{1/2}$ stands for the Hermitian square root of a matrix and \mathbf{H}_{k} is a MIMO channel with independent, uncorrelated and unit variance Gaussian elements at time instant k.

As the correlated channel model (26) is derived from the channel with uncorrelated coefficients, it is possible to formulate the time evolution of spatially correlated channels in a way analog to (25). Then, by defining $\mathbf{h}_k = \text{vec}(\mathbf{H}_k) \in \mathcal{C}^{M_R M_T \times 1}$ as the vector resulting from stacking the columns of \mathbf{H}_k on top of each other, we can express the time-varying AR(1) correlated channel model as [16]

$$\mathbf{h}_{k}^{\text{corr}} = \beta \mathbf{h}_{k-1}^{\text{corr}} + \mathbf{G} \mathbf{w}_{k}, \qquad (27)$$

where $\mathbf{h}_{k}^{\text{COTT}}$ is a vector with spatially correlated channel coefficients at instant k, $\mathbf{G} = \mathbf{R}_{M_{T}}^{1/2} \otimes \mathbf{R}_{M_{R}}^{1/2} \in \mathcal{C}^{M_{R}M_{T} \times M_{R}M_{T}}$ and \mathbf{w}_{k} is $\mathcal{CN}(0, \sigma_{w}^{2}\mathbf{I})$.

It is worth noting that the model in (27) is quite general. For instance, when \mathbf{R}_{M_R} and \mathbf{R}_{M_T} are both diagonal matrices, the channels are spatially uncorrelated and (27) reduces to (25). When there is no relative motion between transmitter and receiver, the maximum Doppler shift f_D equals to zero and, consequently, $\beta = 1$ and $\sigma_w^2 = 0$. In this case, (27) reduces to $\mathbf{h}_k^{\text{corr}} = \mathbf{h}_{k-1}^{\text{corr}}$, i.e., time-invariant channels such as the ones considered previously in Sections III and IV.

B. Channel estimation

Most previous works on space-time coding and antenna selection, such as [4], [5], [11], [22], [24], consider that the channel is perfectly known at the receiver. Unfortunately, in practice this channel information is not normally available. Therefore, channel estimation techniques are essential for MRC receivers to correctly decode the received signals.

In general, channel estimators can be divided into three categories: supervised, unsupervised (or blind) and semiblind algorithms. In supervised channel estimation, a training

(known) sequence is periodically sent to the receiver. By comparing the training sequence to the corresponding received signals, the algorithms are able to estimate the channel. Blind algorithms, on the other hand, do not use any training sequence, basing the estimation purely on the received signals and on the statistical properties of the transmitted signals. For this reason, blind algorithms generally demand more computational power than supervised ones. Finally, semiblind techniques combine characteristics of both supervised and unsupervised algorithms, using not just the training sequence, but also the data symbols to estimate the channel. Since most of the communication systems has some sort of training sequence, we focus only on supervised and semiblind channel estimators.

When the channel is quasi-static, as it was assumed in Sections II, III and IV, methods such as those presented in [3], [17] can be successfully used. In this paper, we consider the minimum mean squared error (MMSE) estimator for quasi-static channel scenarios. This estimator is derived in [3], [17] and its final expression is written as

$$\hat{\mathbf{H}}_{\mathbf{MMSE}} = \mathbf{Y} (\mathbf{P}^H \mathbf{R}_H \mathbf{P} + \sigma_n^2 \mathbf{I})^{-1} \mathbf{P}^H \mathbf{R}_H, \qquad (28)$$

where $\mathbf{P} \in M_T \times \tau$ is the matrix with the training sequences sent by all of transmit antennas, $\mathbf{R}_H \in M_T \times M_T$ is the channel correlation matrix and $\sigma_n^2 \mathbf{I}$ is the noise covariance matrix. In cases where the channel is time-varying, the estimation algorithms must be able to track these channel variations, causing the development of adaptive algorithms. One of the most simple and widely known approaches in adaptive filtering theory is the Least Mean Square (LMS) algorithm [25]. The update equations for the *j*-th receive antenna and *k*-th instant are given by

$$\boldsymbol{\varepsilon}_{j,k} = \mathbf{y}_{j,k} - \mathbf{P}_k^{\mathrm{T}} \mathbf{h}_{j,k}^* \tag{29}$$

$$\mathbf{h}_{j,k+1} = \mathbf{h}_{j,k} + \mu \mathbf{P}_k \boldsymbol{\varepsilon}_{j,k}^*, \tag{30}$$

where μ is the step-size, that controls the converge speed and the final estimation error. The LMS algorithm can operate in both training and decision-directed (DD) modes. In the training mode, pilot (known) symbols are available to the receiver, so the matrix \mathbf{P}_k is known. Once the transmission of the training sequence is finished, the algorithm enters the DD mode (semiblind), where the matrix \mathbf{P}_k is formed by the decisions provided by the MRC decoder. Although this could lead to an error propagation, in this paper we use the simplifying assumption, as in [23], that these decisions are correct.

VI. CODEBOOK DESIGN FOR $M_T = 4NT$, SIMULATION RESULTS AND DISCUSSION

According to new technologies in MIMO systems, which can have much more than four transmit antennas available, we extend the proposed scheme for any number of antennas that is a multiple of four, i.e., $M_T = 4NT$ transmit antennas and $M_R \ge 1$, where $NT \in \mathbb{Z}^*_+$. As described before, the

symbol s should be preprocessed by a complex transmission codeword \mathbf{x} :

$$\mathbf{x} = \frac{1}{\sqrt{M_T/2}} \begin{bmatrix} \cos(\theta)e^{j\varphi_0} \\ \cos(\theta)e^{j\varphi_{l-1}} \\ \vdots \\ \cos(\theta)e^{j\varphi_l} \\ \sin(\theta)e^{j\varphi_0} \\ \sin(\theta)e^{j\varphi_{l+1}} \\ \vdots \\ \sin(\theta)e^{j\varphi_L} \end{bmatrix}$$
(31)

where $l = M_T/2$. The main cost of this extension is the minimum number of feedback bits $b = M_T$ required, which is essential to ensure full diversity of BER performance.

From (1) and (31), the received signal y for M_R receive antennas can be rewritten as

$$\mathbf{y} = \mathbf{H}\mathbf{p} + \mathbf{n}, \tag{32}$$

where

$$\mathbf{H}\mathbf{p} = s\mathbf{H}\mathbf{x} = \bar{\mathbf{h}}, \\ \bar{\mathbf{h}} = s[h_{p1} \dots h_{pM_R}]^{\mathrm{T}},$$

in which

$$h_{pj} = \cos(\theta)h_{1,j} + \cos(\theta)e^{\varphi_1}h_{2,j} + \cdots + \cos(\theta)e^{\varphi_{l-1}}h_{(M_T-3),j} + \cos(\theta)e^{\varphi_l}h_{(M_T-2),j} + \sin(\theta)h_{3,j} + \sin(\theta)e^{\varphi_2}h_{4,j} + \cdots + \sin(\theta)e^{\varphi_{L-1}}h_{(M_T-1),j}\sin(\theta)e^{\varphi_L}h_{M_T,j}.$$

Considering the received signal in (32) and employing the MRC technique, the following processing produces the desired inputs to the maximum-likelihood detector:

$$\tilde{s} = s\left[\left(\sum_{j=1}^{M_R} (|h_{1,j}|^2 + \dots + |h_{l,j}|^2) + \sum_{j=1}^{M_R} \beta_{Cj}\right) \cos^2(\theta) + \left(\sum_{j=1}^{M_R} |h_{l+1,j}|^2 + \dots + |h_{L,j}|^2) + \sum_{j=1}^{M_R} \beta_{Sj}\right) \sin^2(\theta) + \sum_{j=1}^{M_R} \beta_{CSj} \cos(\theta) \sin(\theta) \left]\sqrt{\rho}/2 + \sum_{j=1}^{M_R} H_{pj}^* \eta_j, \quad (33)$$

where

$$\beta_{Cj} = \sum_{m=1}^{l-1} \sum_{n=1}^{l-1} 2\Re\{g_{m,j}g_{n,j}^*\},\$$

$$\beta_{Sj} = \sum_{m=l}^{L} \sum_{n=l}^{L} 2\Re\{g_{m,j}g_{n,j}^*\}, m \neq n,\$$

$$\beta_{CSj} = 2\Re\{(g_{1,j} + \dots + g_{l/2,j}) \times (g_{l/2+1,j} + \dots + g_{L,j})^*\},\$$

$$\mathbf{G} = \mathbf{H} \odot \mathbf{V}_{ij}$$

$$= \begin{bmatrix} e^{j\varphi_0} \dots e^{j\varphi_l} & e^{j\varphi_0} & e^{j\varphi_{l+1}} \dots e^{j\varphi_L} \\ \vdots & \vdots & \vdots \\ e^{j\varphi_0} \dots e^{j\varphi_l} & e^{j\varphi_0} & e^{j\varphi_{l+1}} \dots e^{j\varphi_L} \end{bmatrix}.$$
 (34)

 $V_{\varphi} =$

In this section, we present the simulation results used to assess the performance of the proposed scheme. We also compare the obtained BER performance of the proposed scheme with other two closed-loop codebook-based schemes with four transmit antennas: the extended orthogonal spacetime block code scheme (EO-STBC) [9], the Alamouti-code based scheme (ACBS) [11] and the DFT [14]. For the simulations, we assume that the symbols are mapped into a QPSK constellation, the receiver sends b bits over an error-free and zero-delay feedback channel, and the stopping criterion is the occurrence of 300 symbol errors per average SNR. The BER performance for the no-diversity scenario (singleinput single-output scheme) is also plotted in Fig. 1, used as a reference curve. The performance results are compared in terms of bit error rate (BER) versus ρ over quasi-static flat Rayleigh fading channels.

In Figs. 1 (a) and (b), results are given for $M_T = 4$ transmit antennas and $M_R = 1$ receive antenna. Fig. 1 shows the BER performance of the proposed, the EO-STBC and the ACBS schemes. For Fig. 1 (a), we assumed that there is an ideal (unquantized) feedback channel between transmitter and receiver in order to assess the best performance that can be reached by the schemes. We can observe that the proposed scheme achieves diversity order of $M_T M_R = 4$ (the same order achieved by the other ones) and has a performance gain of about 3dB ($b = \infty$) and 1.3dB (b = 3) over the other schemes.

In Fig. 2 we compare the BER performances of the proposed codebooks to that of the uniform DFT codebook presented in [14]. The DFT and the proposed scheme have approximately the same BER performances for $M_T = 4$, $M_R = 1$, and b = 4 feedback bits. However, as the number of feedback bits is increased, the proposed scheme presents a considerable BER improvement, while the DFT one has just a little performance gain. The codebook presented in [14] offers a good BER performance for a limited quantized feedback channel. A drawback of this solution is the BER performance saturation imposed by the orthogonality of the DFT, which is not observed in our proposal since the codebook design is optimized for quasi-orthogonal codes. Additionally, those solutions have the same design complexity since in both cases the codebooks are based on trigonometrical functions.

Figure 3 (a) presents the theoretical upper bounds for the proposed scheme with $M_T = 4$, $M_R = 1$ and $M_R = 2$. We have considered the codebooks \mathbf{X}_8^4 for b = 3 and \mathbf{X}_{16}^4 for b = 4 (see Table I and II for more details). We can note that the simulated and theoretical performances get closer and closer as the number of feedback bits is increased because of the approaches we adopted for the derivations. Fig. 2 (b) illustrates the BER performance for an extended version of the proposed scheme. In this case, the scheme has $M_T = 8$ antennas, for b = 7, 8 and the codes follow the same rule as was described earlier. More details about this extended scheme



Fig. 1. BER performances for $M_T = 4$ and $M_R = 1$ for the EO-STBC [9], ACBS [11] and the proposed schemes (a) assuming a unquantized feedback channel $(b = \infty)$, (b) assuming a quantized feedback channel with b = 3.



Fig. 2. BER performances for $M_T = 4$ and $M_R = 1$ for the DFT [14] and the proposed scheme assuming a quantized feedback channel with b = 3, 4 and unquantized feedback.

will be presented in the next section. As one can see, the diversity order of $8M_R$ is obtained in both cases.

Figures 4 (a) and (b) state the performance of the proposed scheme for a scenario with fast flat fading. The length of the training sequence takes 25% of the whole transmit frame. For these cases, all of the simulations have used b = 3. In Fig. 4 (a), we assess the BER performance of the proposed scheme for both the LMS and MMSE estimators at the receiver. We have assumed a relative velocity of 100km/h in both scenarios. As a result, the LMS estimator provided a better performance when compared with the MMSE.

We evaluate the robustness of the proposed scheme by adding spatial correlation in the simulations. Thus, in Figs. 5 (a) and (b) we evaluate the BER performance when the communication is simultaneously affected by the Doppler

TABLE III BER PERFORMANCE OF THE PROPOSED SCHEME UNDER DOPPLER EFFECT AND SPATIAL CORRELATION. IT WAS ASSUMED $\rho=15~dB$

Doppler	BER	Correlation C	BER
0 km/h	$10^{-4.9}$	0	$10^{-4.9}$
5 km/h	$10^{-4.8}$	0.2	$10^{-4.7}$
50 km/h	$10^{-4.4}$	0.3	$10^{-4.7}$
100 km/h	$10^{-3.8}$	0.5	$10^{-4.5}$
150 km/h	$10^{-3.1}$	0.8	$10^{-3.6}$

effect and the spatial correlation. Again, we have assumed a relative velocity of 100 km/h and b = 3. Additionally, in Fig. 5 (b), we have considered two different level of spatial correlation, i.e., C = 0.2 and C = 0.5. Based on the results, we can assert that the proposed scheme presents a better BER performance when compared to the ACBS for different channel conditions. More details on these results can be found in Table III.

Note that in this paper we focus our attention in how to explore the spatial diversity available at radio base stations for wireless communications without add much complexity in the system. In terms of real-world scenarios, one can boost this potential by simply dividing a cell into multiple sectors, thus increasing network capacity, such as in multilayer sectorization [26], where the transmit antennas are distributed into the sectors, where the proposed scheme can still be considered as a good solution.

Regarding the results presented in the simulation results, we showed that the proposed scheme keeps a good bit error performance for scenarios with low correlation and low Doppler. The performance degradation presented for either high Doppler or high spatial correlation can be easily explained. For high spatial correlation at the transmitter the orthogonal structure is lost, which is undesirable, since the proposed scheme explores the "quasi-orthogonal" structure of



Fig. 3. BER performances comparing the upper bound to the simulations (a) $M_T = 4$, $M_R = 1$ and $M_R = 2$ (b) $M_T = 8$, $M_R = 1$ and b = 7, 8.



Fig. 4. Performance comparison of the proposed scheme (a) for the LMS and MMSE channel estimators, (b) the LMS with different relative velocities.



Fig. 5. BER performance of the proposed scheme by using the LMS estimator (a) while varying the spatial correlation level C, (b) as compared to the ACBS scheme[11].

the codes. The high mobility makes the channel estimation less accurate, and, as a result, more cross terms will appear in the SNR expression which can not be controlled by the proposed model. For the fast fading scenario the performance of the proposed scheme can be improved by using the estimator based on the Kalman filter [27], for instance.

VII. CONCLUSIONS AND FINAL REMARKS

A low-complexity codebook-based beamforming with quantized feedback channel was proposed. The proposed scheme is based on a preprocessing that combines the phase rotation and power allocation (suboptimal in this proposal), culminating into a new simple codebook transmission scheme. The proposal can be seen as a code selector scheme, which allows us to evaluate it as a codebook-based design. An instantaneous SNR analysis was addressed in order to find the optimal feedback to be sent to the transmitter. The proposed scheme was evaluated in terms of BER performance through Monte Carlo simulations. Further, a quantized feedback analysis over quasi-static flat Rayleigh fading channels was considered, and an upper bound on the BER performance was derived. The proposed scheme was evaluated for other more realistic scenarios, where we have assumed a spatial correlation at the transmitter and relative mobility between transmitter and receiver. The results showed that the proposed scheme keeps a good bit error performance for scenarios with low correlation and low Doppler. Finally, we have presented how to extend the proposed codebook design to any MIMO system with $M_T = 4N$ antennas.

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